

A BiCMOS Ultra-Wideband 3.1-10.6GHz Front-End

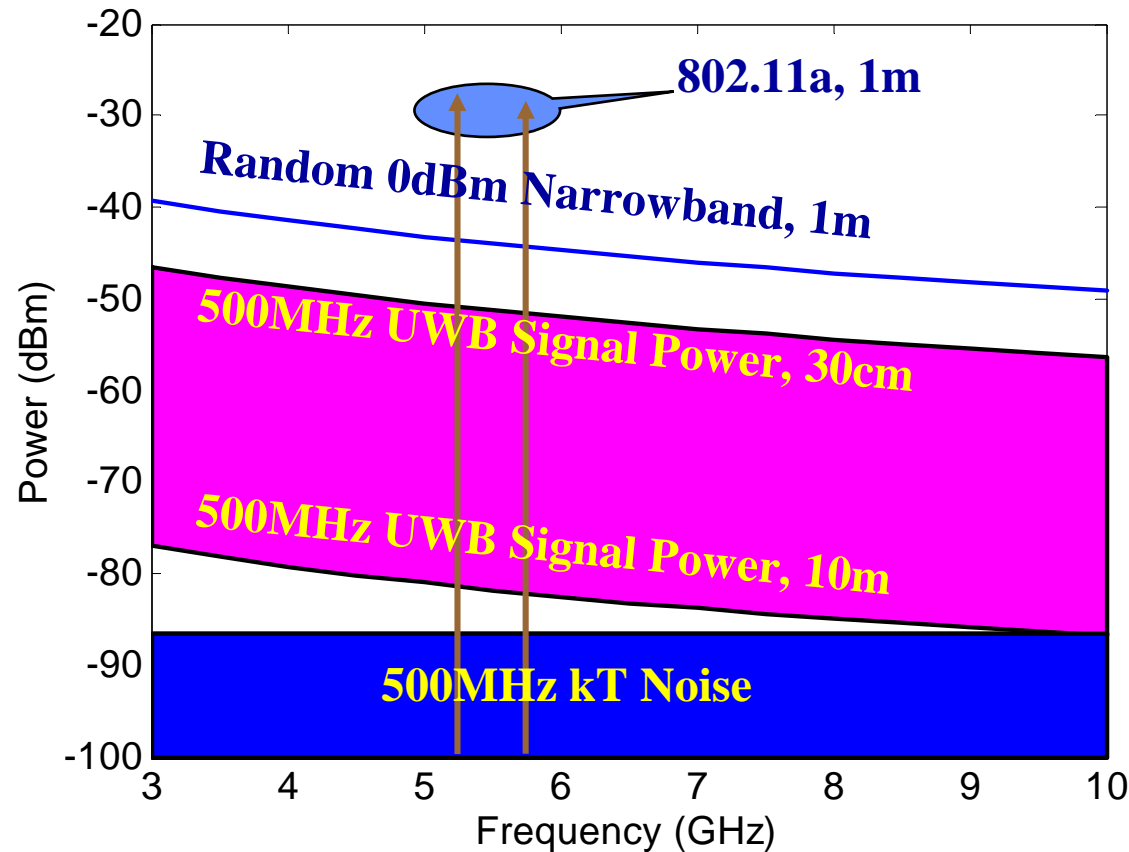
Fred S. Lee and Anantha P. Chandrakasan
Massachusetts Institute of Technology
Cambridge, MA

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Outline

- **UWB Wireless Channel Characteristics**
- **Receiver Architecture**
 - **Matching**
 - **Single-to-Differential Converter w/Notch**
- **Circuit Design**
- **Measurement Results**
- **Conclusions**

UWB Wireless Channel Characteristics



Signals	Power @ TX	TX-RX Distance	Power @ RX	V _{ampl} @ RX
500MHz UWB @ 3.35GHz	-14dBm	30cm	-47dBm	2.6mV
500MHz UWB @ 10.35GHz	-14dBm	10m	-87dBm	26 μ V
802.11a @ 5.25GHz	15 dBm	1m	-29dBm	10mV
Random @ 3.1GHz	0 dBm	1m	-39dBm	3.2mV

S. Ghassemzadeh, et al., "UWB indoor path loss model for residential and commercial buildings," VTC 2003

Design Specifications

Noise Figure

NF < 4.5 dB

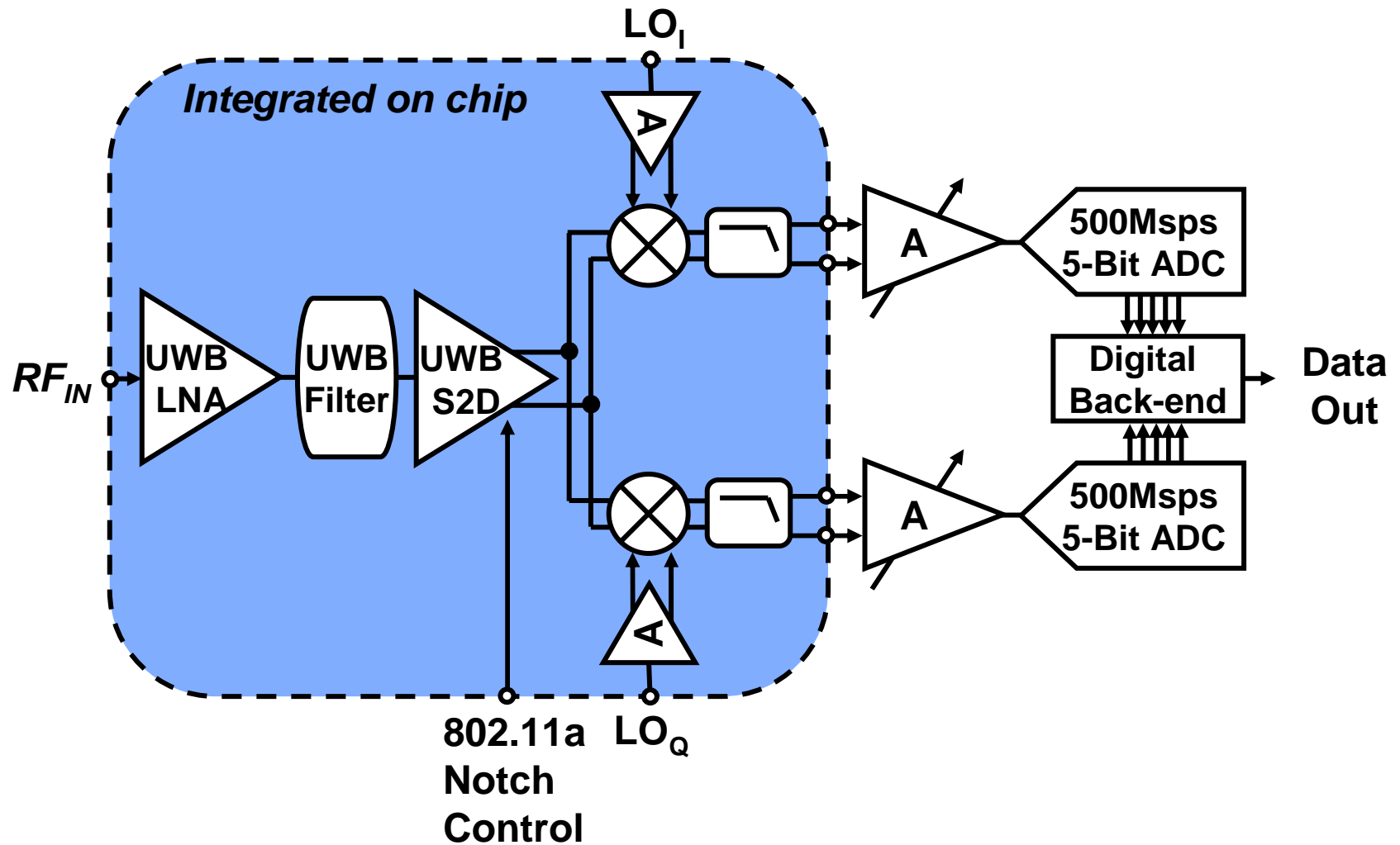
Dynamic Range

For +/-200mV ADC input range, minimum gain = 32dB

Linearity

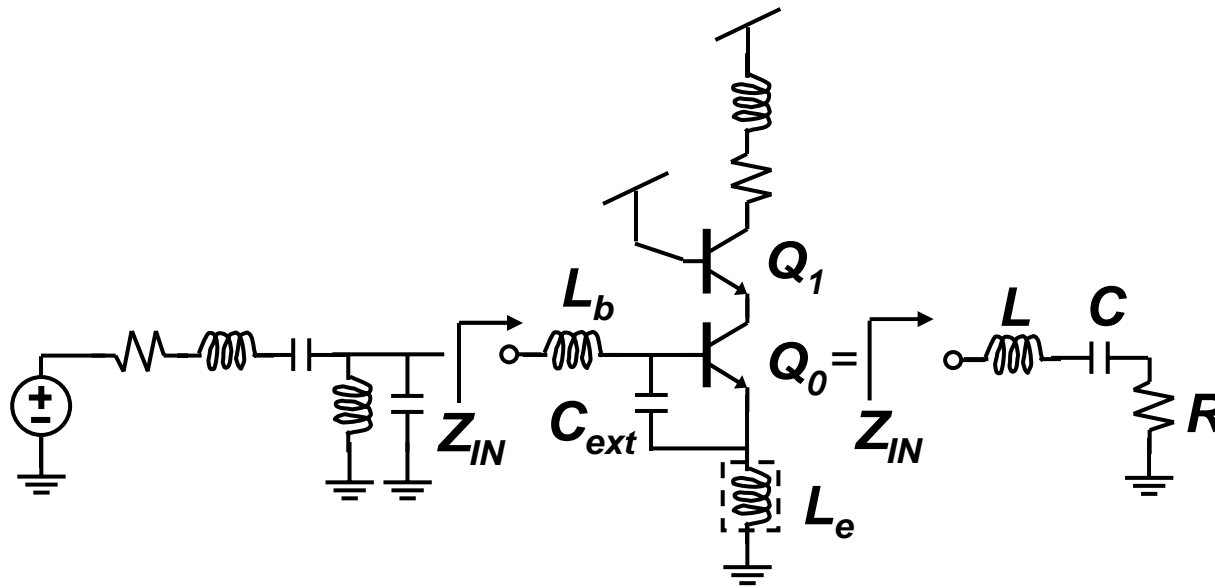
P1dB > -30dBm

Receiver Architecture



Wideband LNA – Ladder Matching

Wideband LNA – ladder match (Ismail, et al., “A 3-10GHz low-noise amplifier with wideband LC-ladder matching network,” JSSC 2004)



$$L = L_b + L_e$$

$$R = \frac{g_m L_e}{C} = 2\pi f_t L_e$$

$$C = C_\pi + C_\mu + C_{ext}$$

$$g_m = 0.067 \quad C_\pi = 170 \text{ fF}$$

Achieves close to NF_{min} for NF and power match

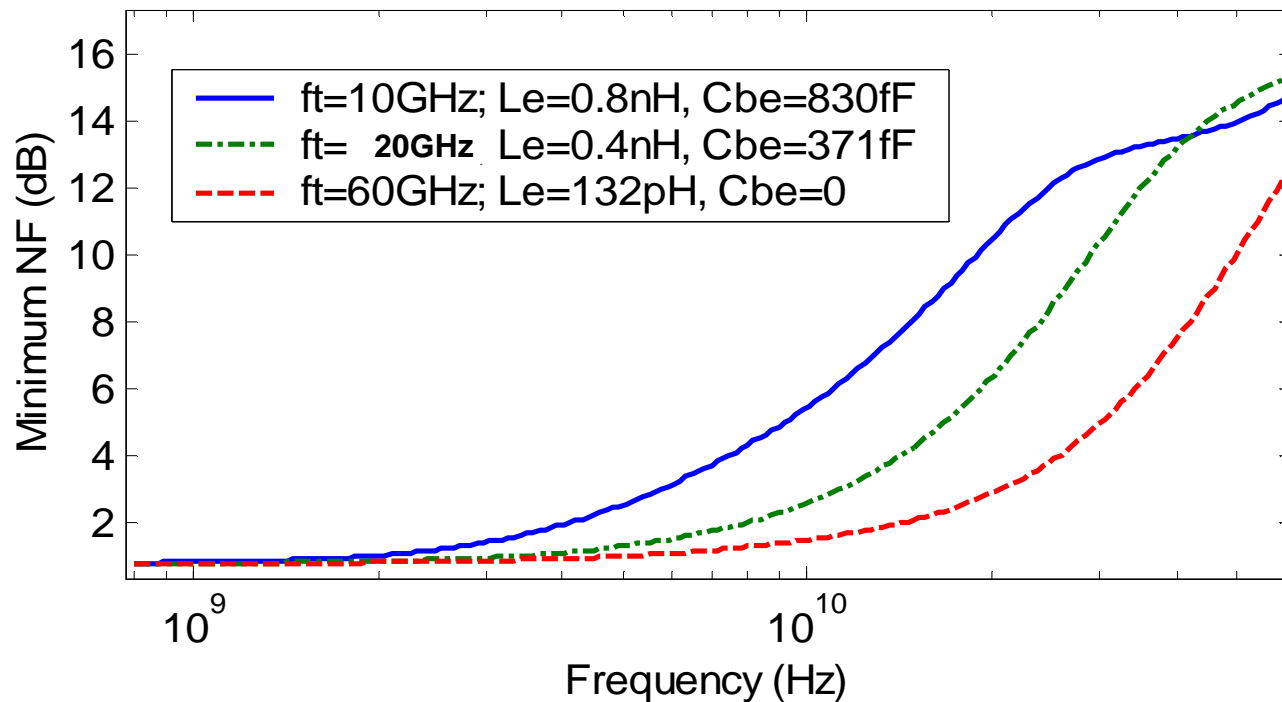
R formed by $g_m L_e / C$, and other LC components keep S_{11} within -10dB across the bandwidth of interest

Wideband LNA – NF_{\min} and f_t Tradeoff

NF_{\min} equation:
$$NF_{\min} = 1 + \frac{1}{\beta} + \sqrt{2g_m r_B} \sqrt{\frac{1}{\beta} + \left(\frac{f}{f_t}\right)^2}$$

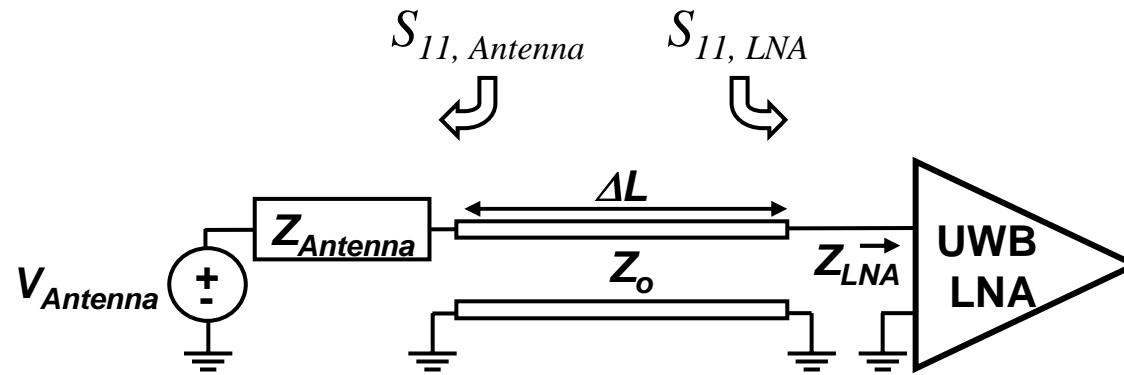
To keep $R = \frac{g_m L_e}{C} = 2\pi f_t L_e$ constant with $L_e \uparrow$, C_{ext} of C must \uparrow to $\downarrow f_t$.

With $f_t \downarrow$, R is constant, but $NF_{\min} \uparrow$!



Operate LNA at high f_t to minimize NF_{\min} and noise match at 10GHz

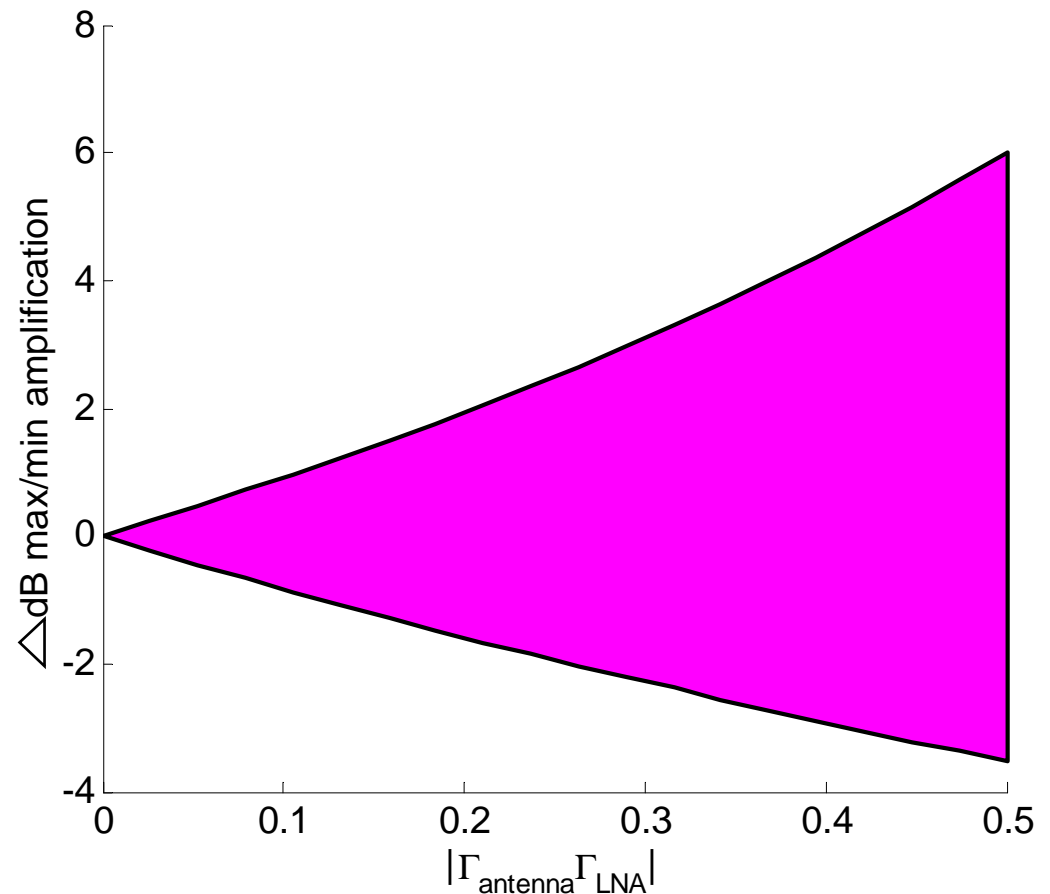
Reflections in Un-Matched Environment



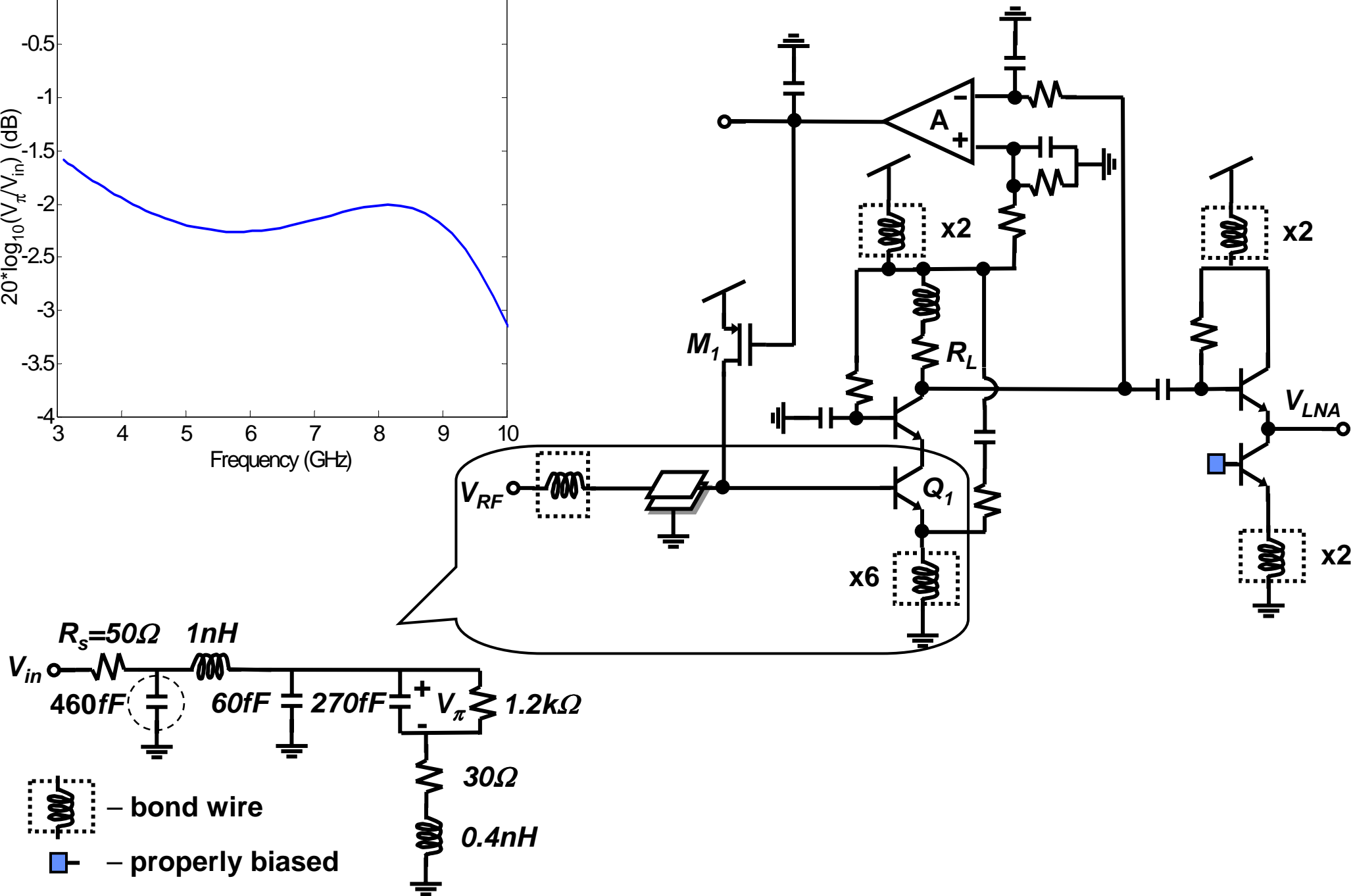
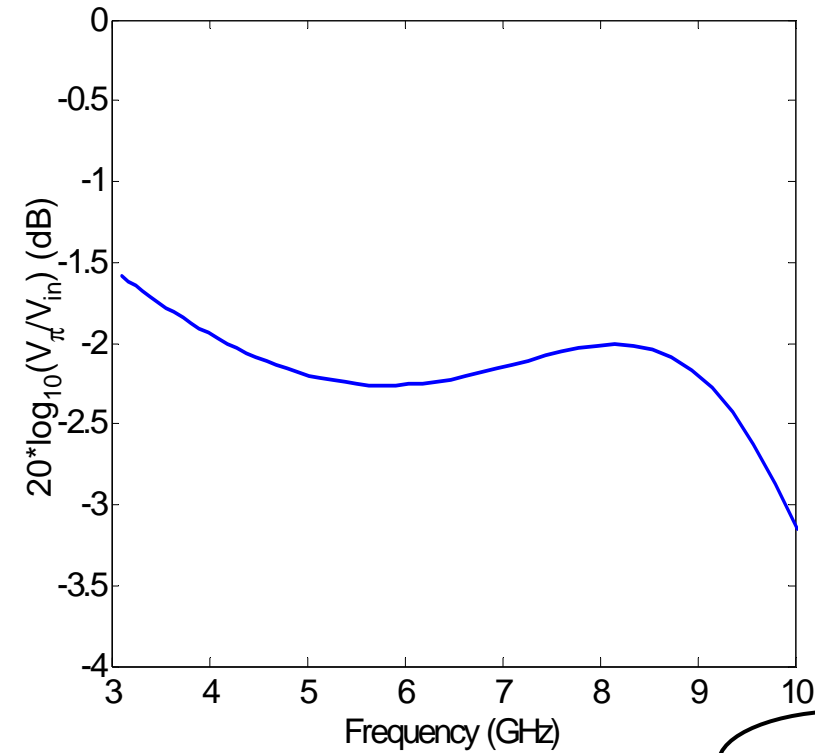
$$A_{\max} = \left(1 - L^2 \left| S_{11, Antenna} \right| \left| S_{11, LNA} \right| \right)^{-1}$$

$$A_{\min} = \left(1 + L^2 \left| S_{11, Antenna} \right| \left| S_{11, LNA} \right| \right)^{-1}$$

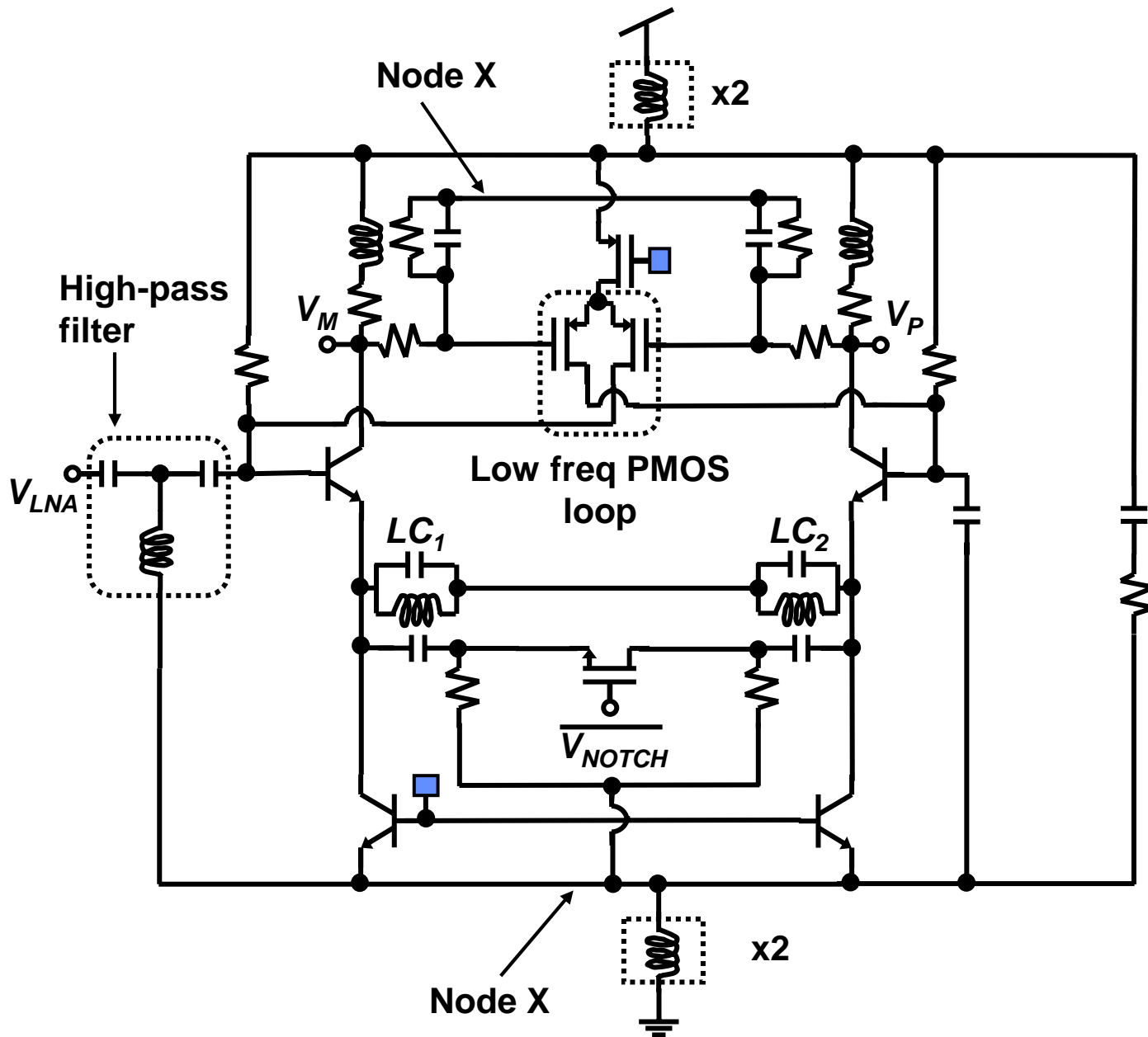
L is loss; if $L = 1$, TX line is lossless



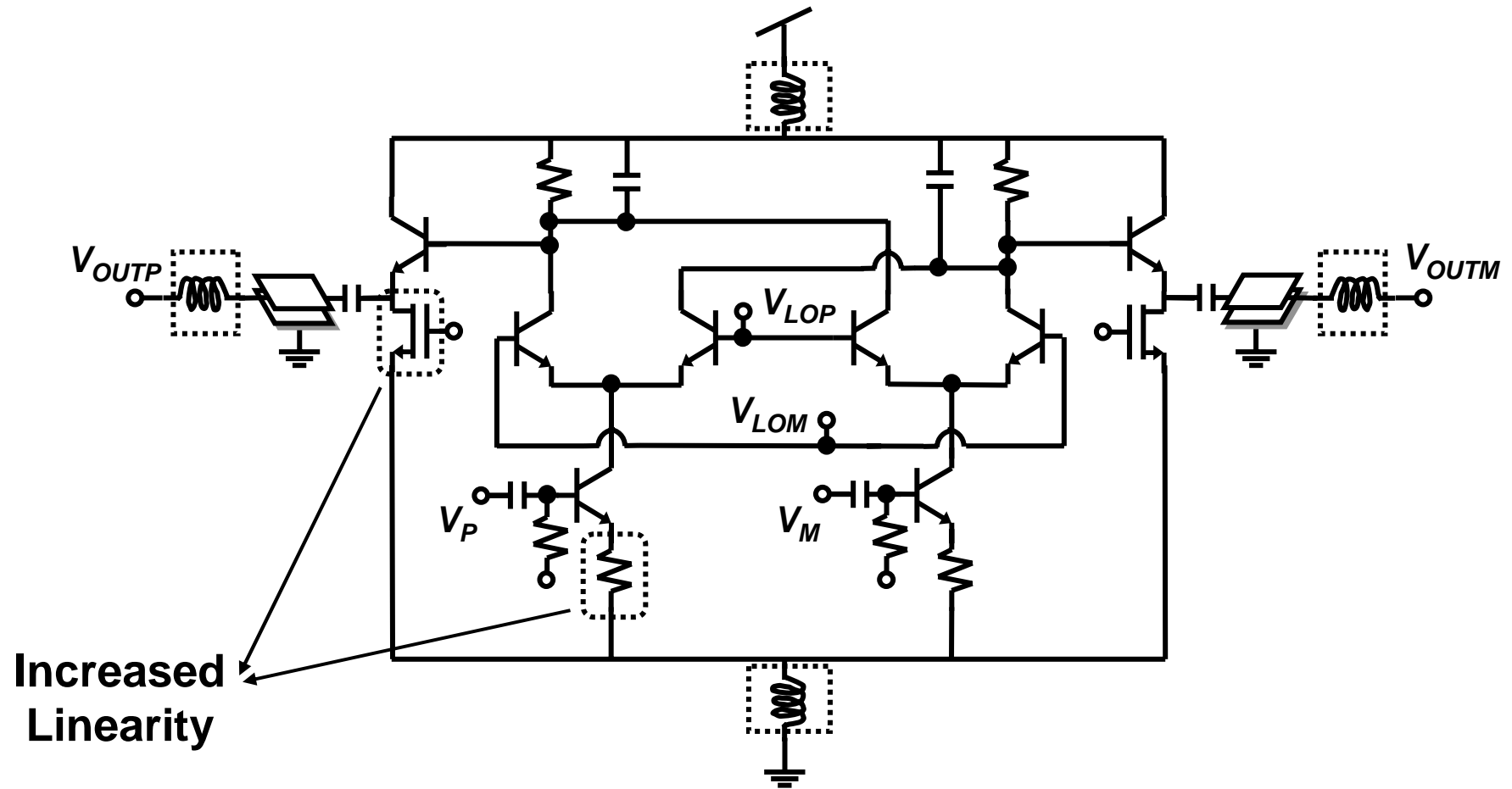
Circuits – LNA Schematic



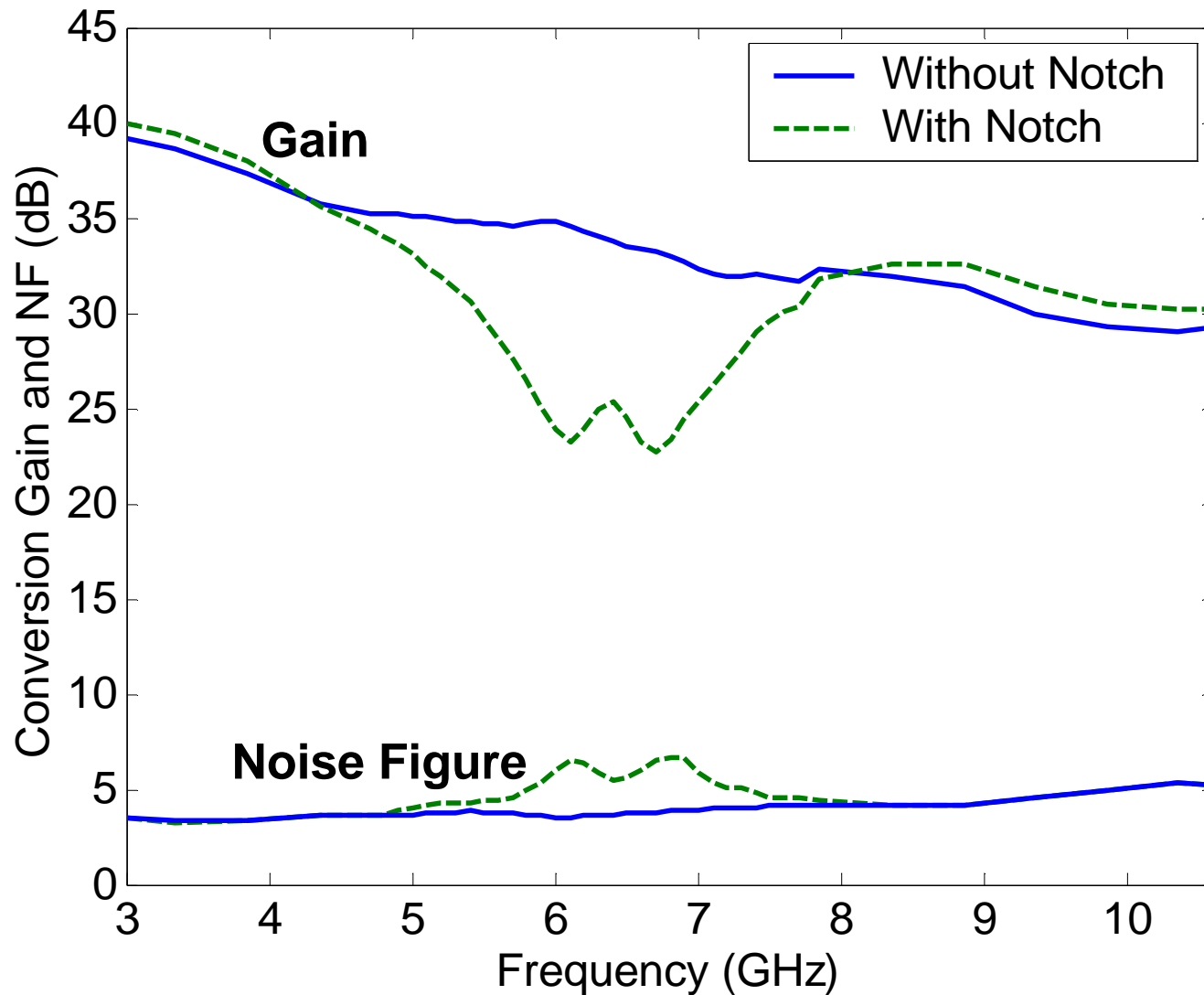
Circuits – UWB Filter and S2D



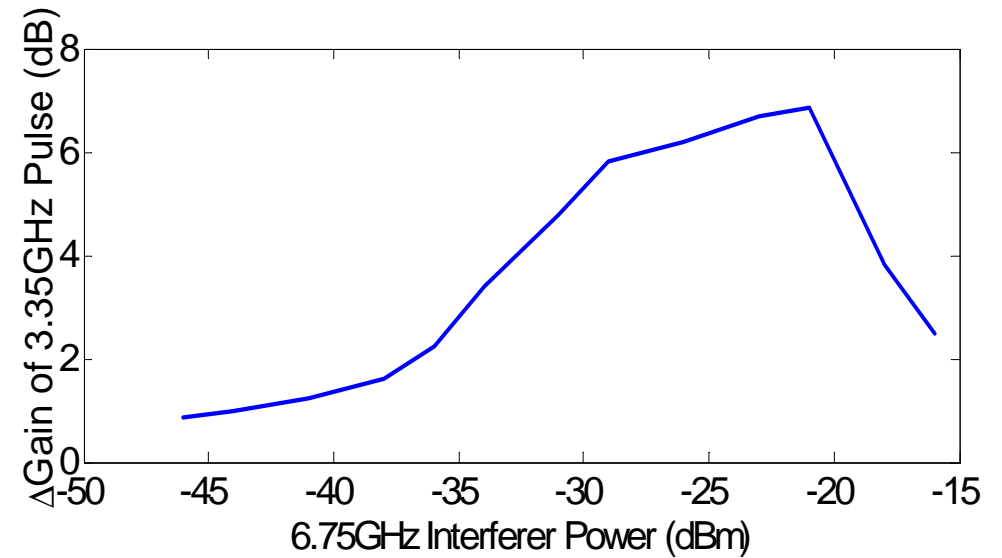
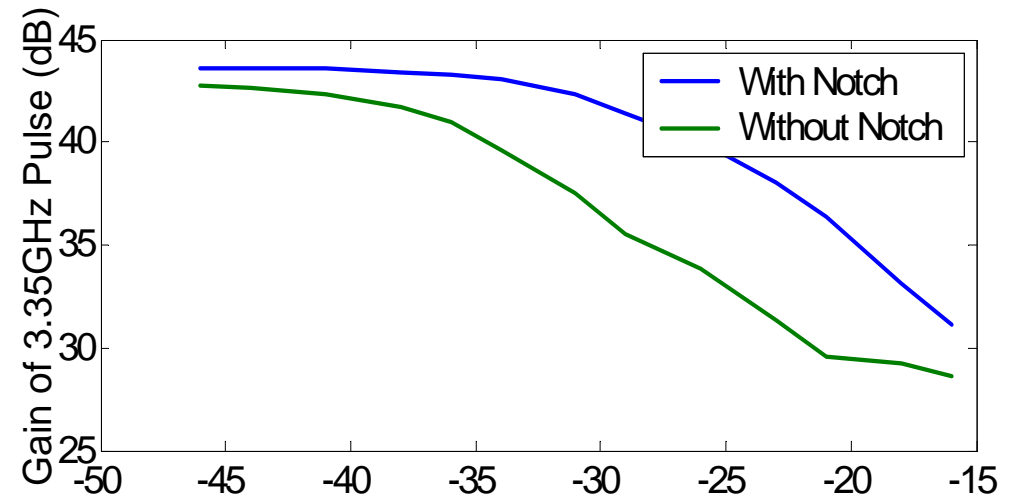
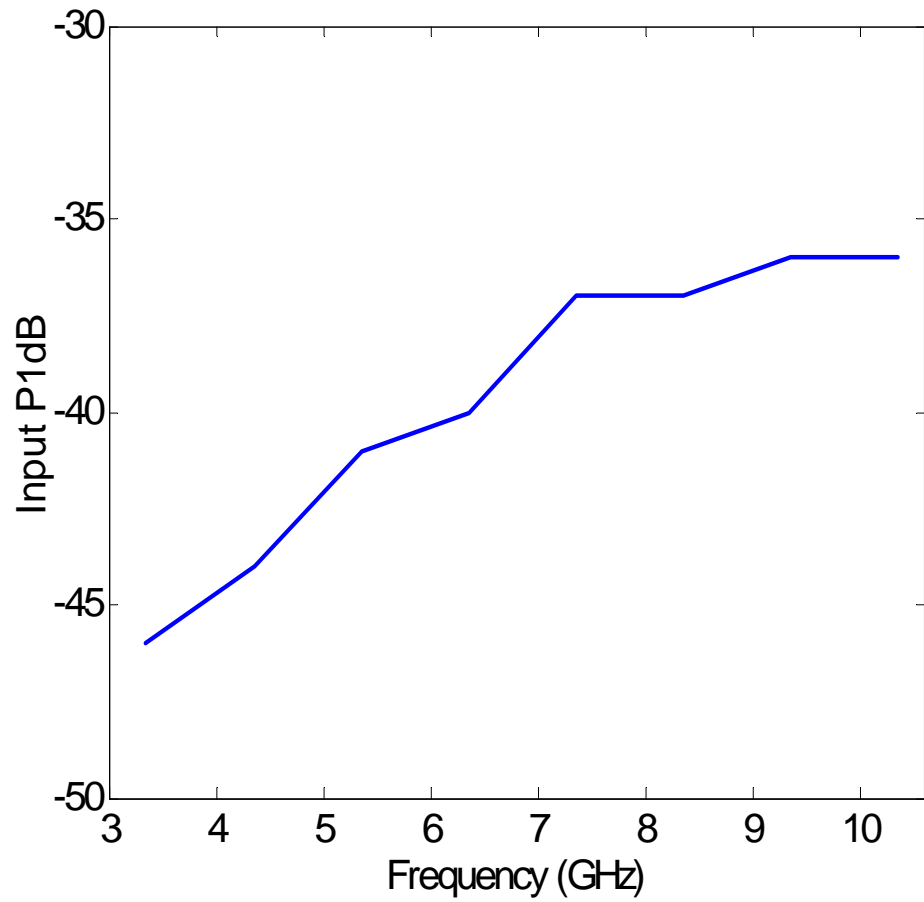
Circuits – Double-Balanced Gilbert Mixers



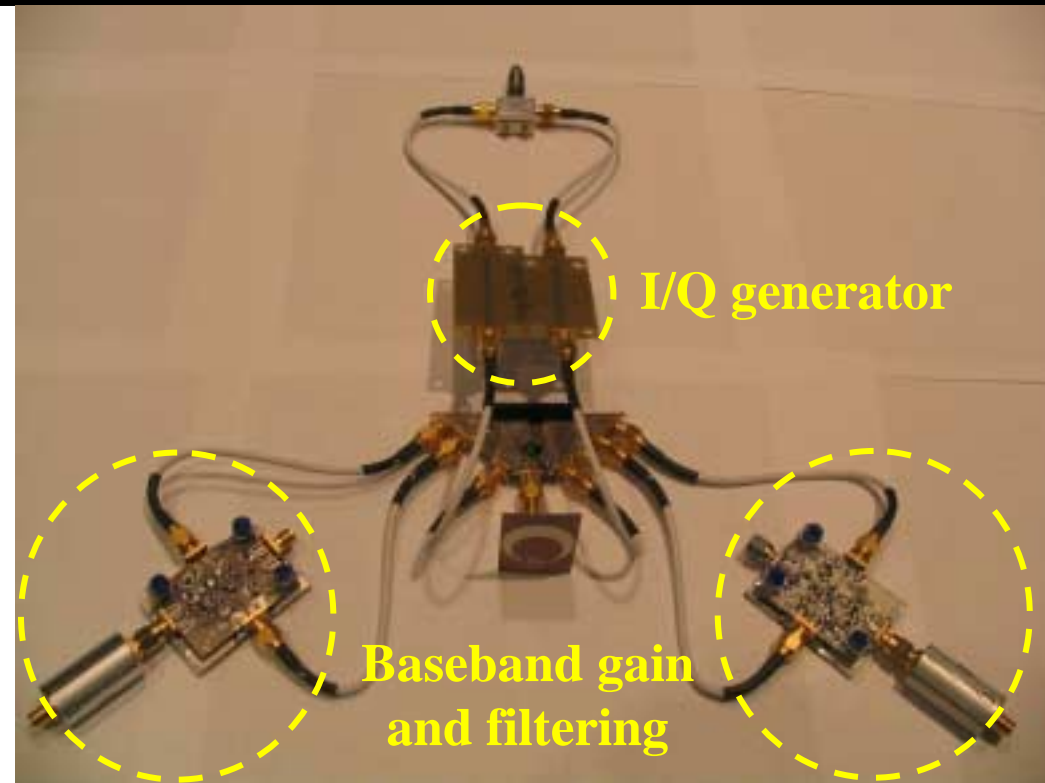
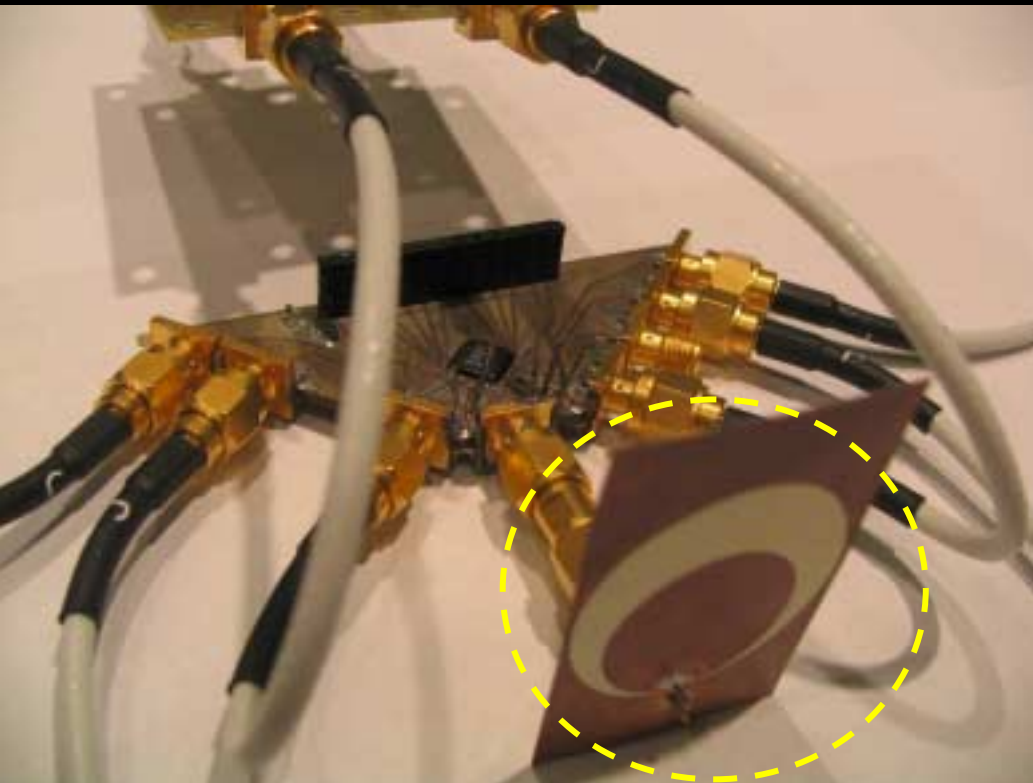
Wired Measurements – Conversion Gain and NF



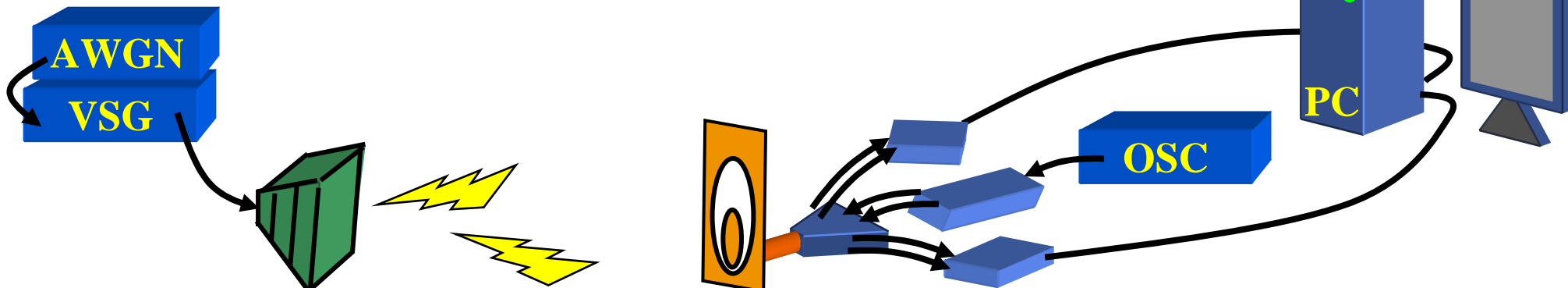
Wired Measurements – Notch Effectiveness



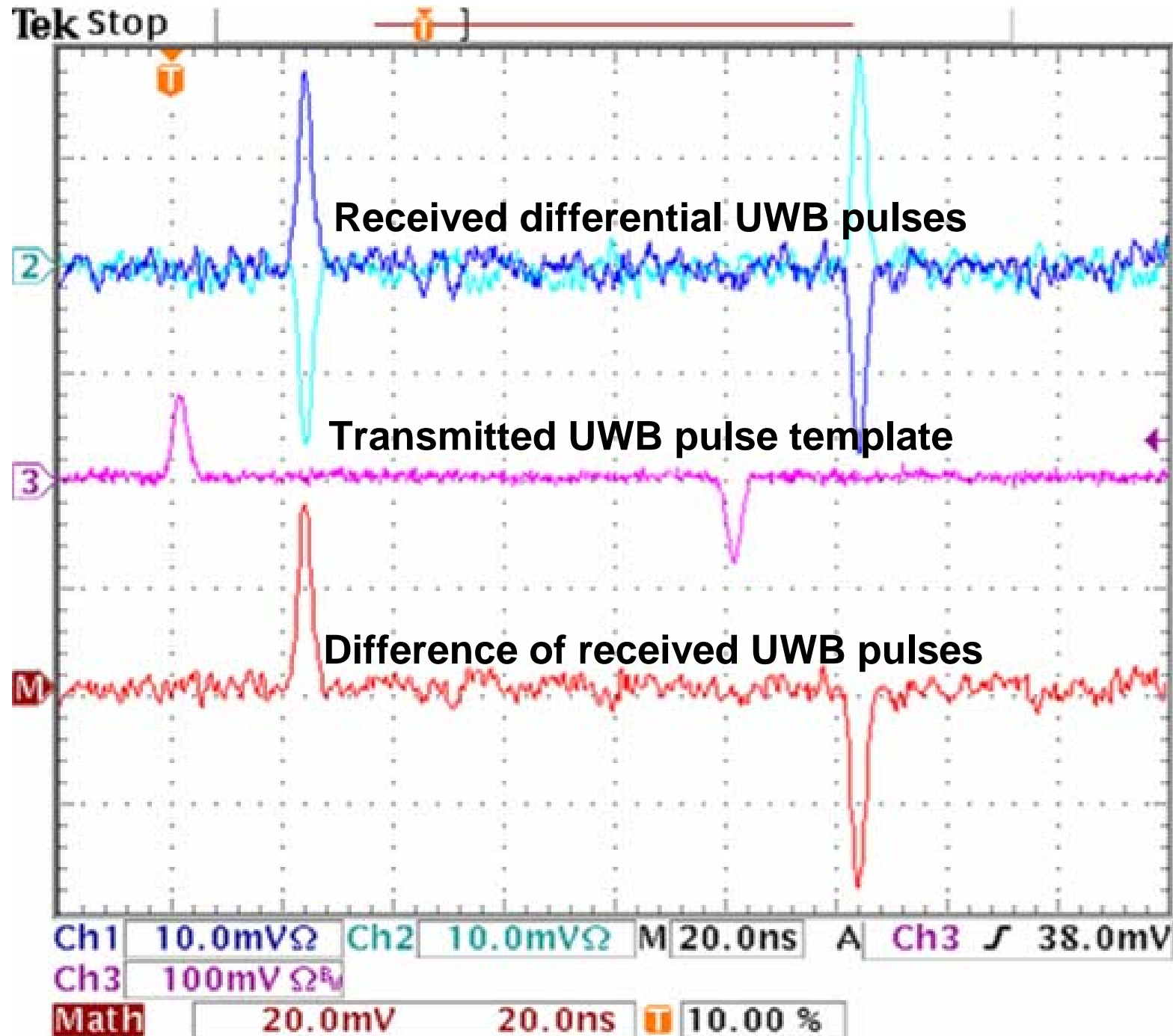
Wireless Measurements Setup



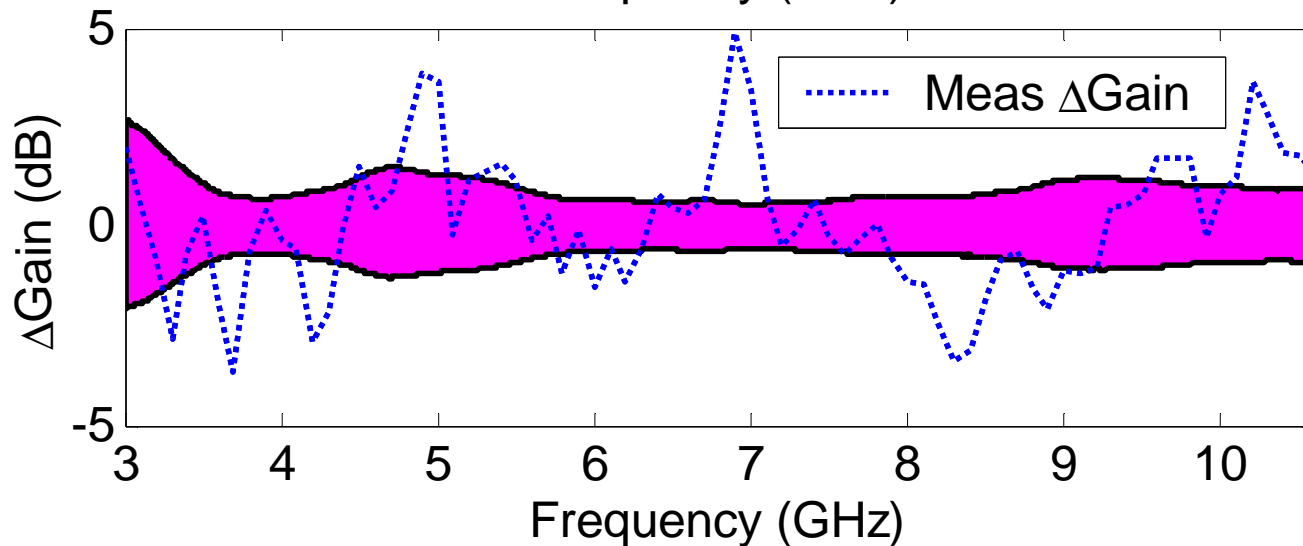
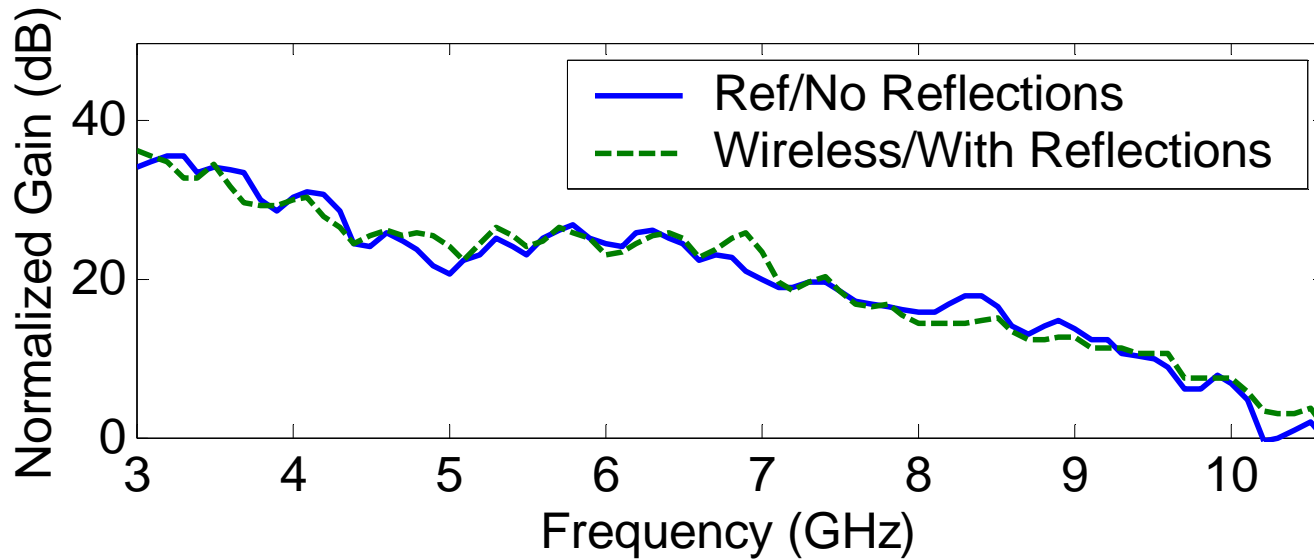
Powell, et al., "Differential and single ended elliptical antennas for 3.1-10.6GHz ultra-wideband communication," APSS 2004



Wirelessly Received UWB Pulse Signals



Wireless Verification of Un-Matched Front-End



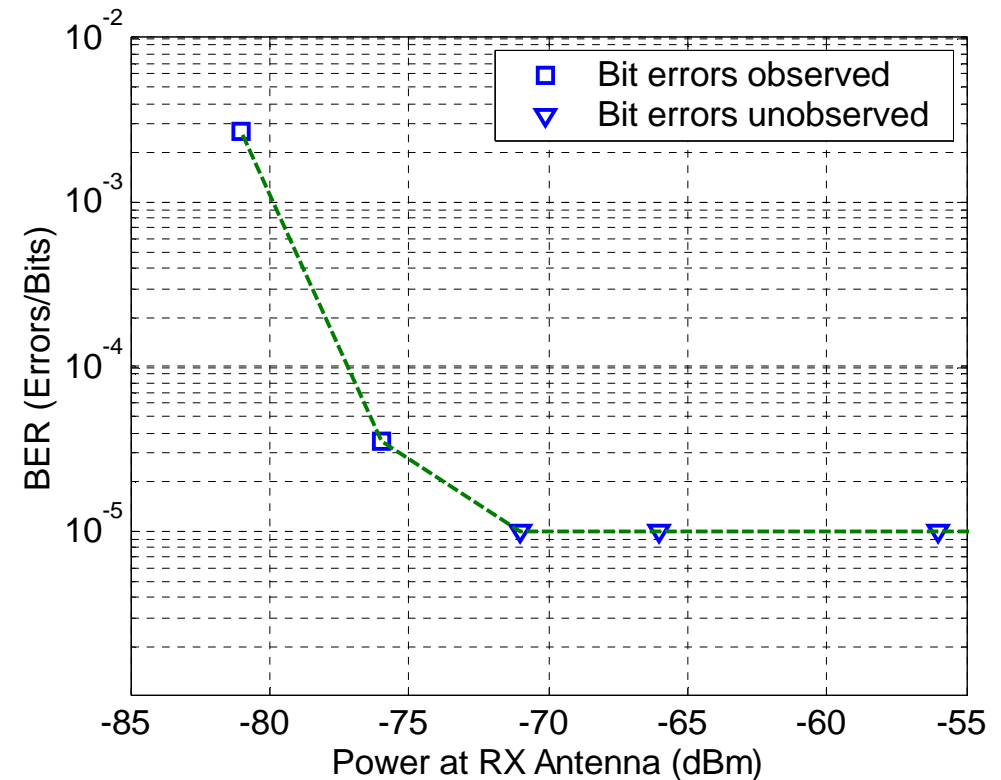
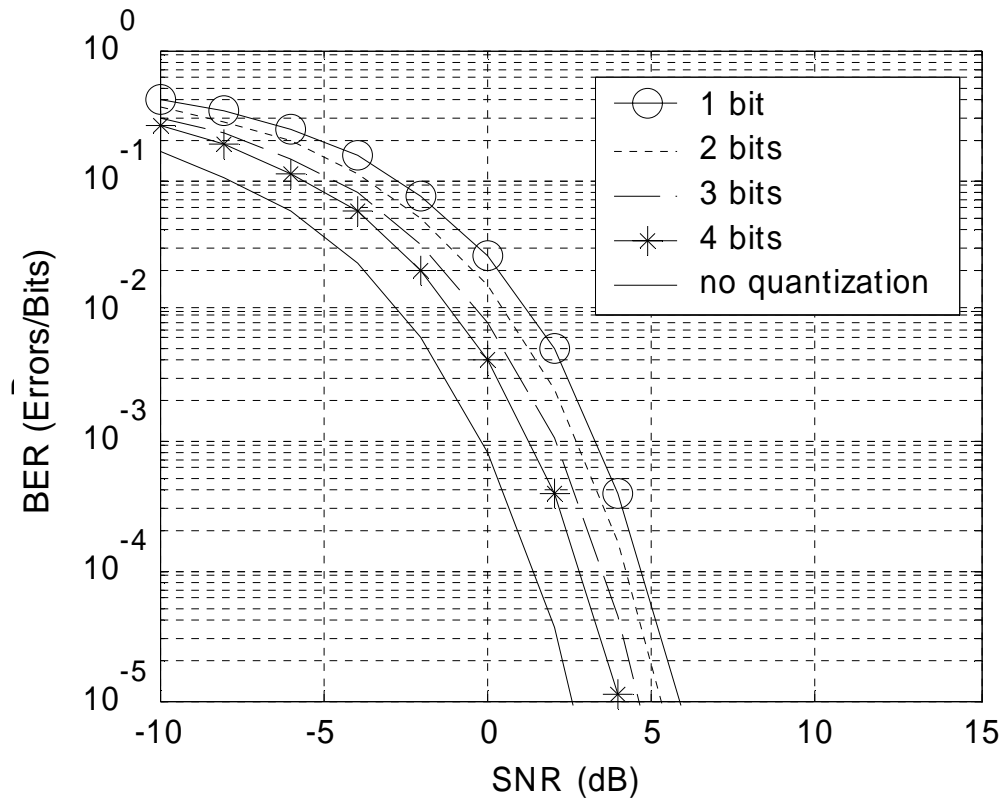
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$$A_{\min} = \left(1 + L^2 |S_{11, Antenna}| |S_{11, LNA}|\right)^{-1}$$

Ref obtained by piecing together the gains of:

- TX/RX antennas path loss, when antennas are driven and loaded with properly matched impedance
- RFIC conversion gain when driven by a matched source

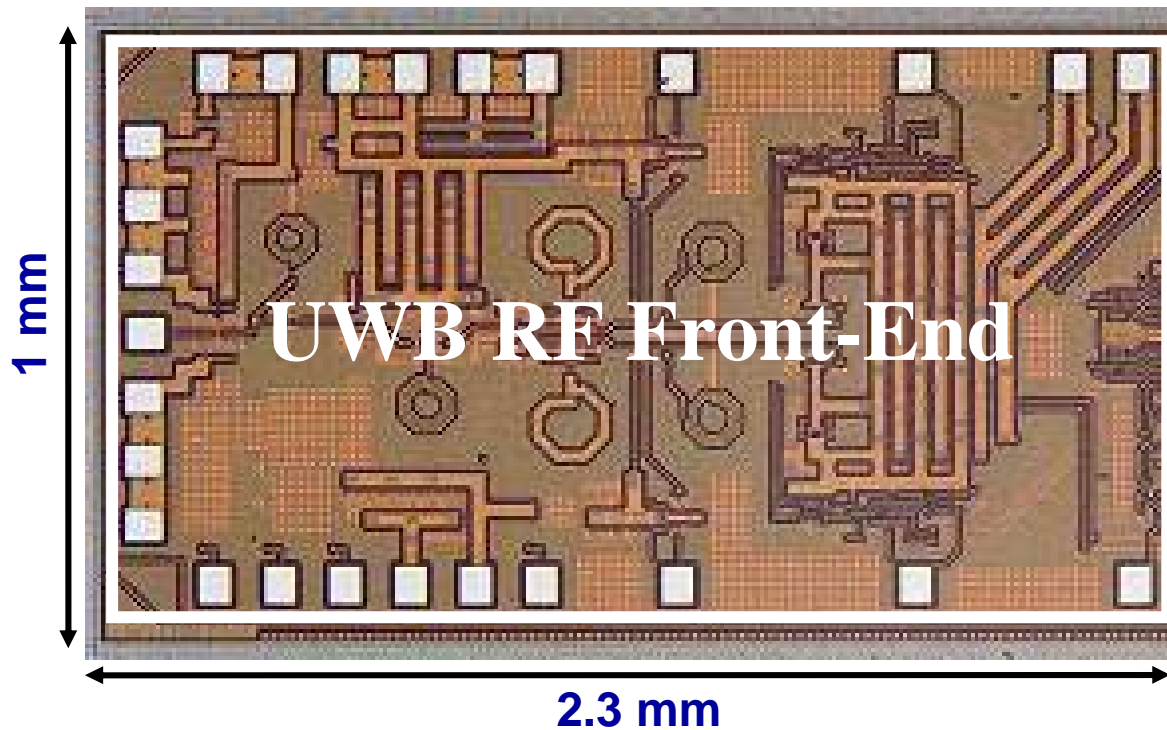
Wireless Bit-Error-Rate Results @ 6.85GHz



Blazquez, et al., "Digital architecture for an ultra-wideband radio receiver," VTC 2003

- To compare plots, change "Power at RX Antenna" to "SNR" by:
 - Assuming kTB in 500MHz band is -87dBm
 - $SNR = dBm_{RX} - 87 + NF$
- We find that these plots match within 2-3 dB

Chip Photo and Performance Summary



Front-End RFIC Summary

Specification	Value from 3.1-10.6GHz
Conversion Gain	39 to 29dB
NF	3.3 to 5dB
Input P1dB	-46 to -36dBm
Notch Filter Attenuation	10dB
BER @ sensitivity	2.7×10^{-3} @ -81dBm
Process technology	0.18 μ m SiGe BiCMOS

Power Consumption at 1.8V

Block	Power (mW)
LNA	4.23
Buffer, S2D & notch	13.5
2 mixers and buffers	21.6
2 LO amplifiers	14.4
Total	53.73

Conclusions

- **Un-matched LNA can achieve better noise performance**
- **RF notch filter can improve robustness to interference**
- **UWB packaged chip verified in wireless system environment**